

REMARKS

Reconsideration and allowance of the subject application in view of the foregoing amendments and the following remarks is respectfully requested. The above amendments are requested to be entered under Rule 116 in that they have been called for by the Examiner in this Office Action and further in that place this application in condition for allowance.

IDS

It is noted that the IDS filed on June 6, 2005 has not yet been acknowledged. Correction of this oversight is respectfully requested in any further action taken.

In the specification/Claims

Most of the corrections noted by the Examiner have been implemented in the form of a Substitute Specification appended to this submission. However, in connection with the gearbox unit 42 and the Figure 10, it is submitted that Figure 10 best shows the connection between elements 47 and 45. Indeed, this connection cannot be seen in Figs. 8 and 9. Therefore no correction has been made.

The reference label F (Fig. 15) was changed to F' in the last response.

Claim 16 was amended in the last response to correct the antecedent basis raised in connection with the "motor mounting plate." The suggested correction to claim 22 was not made in that it was deemed unnecessary. The correction wherein the comma is removed is deemed sufficient.

The status identifier of claim 23 is deemed to be both currently correct and to correct the previous erroneous identification.

Claim amendments/Status

In this response claims 1, 2, 5, 18, 20, 22-25 have been amended to obviate the issues raised in from the third last line of page 2 to line 6 of page 4.

Claim 16-19, 23 have been indicated as being allowable if rewritten to overcome the rejection(s) under 35 USC 112, 2nd paragraph, set forth in this Office action and to include all of the limitations of the base claim and any intervening claims. However, it is deemed premature /unnecessary to limit the claimed subject matter in this manner.

Claims 1-31 remain pending in the application.

Rejections under 35 USC § 112

The rejections of claims 2-6, 16-19, 23-26 under 35 USC 112, second paragraph, as being indefinite for failing to particularly point out and distinctly claim the subject matter which applicant regards as the invention, are submitted as being overcome by the amendments discussed *supra*.

Rejections under 35 USC § 103

The rejections of:

- 1) claims 1, 7, 8, 20 under 35 USC 103(a) as being unpatentable over Nishikawa et al. (Nishikawa) in view of newly cited Yamakawa et al. (Yamakawa);
- 2) claims 9, 12, 13, 15, 24-26 under 35 USC 103(a) as being unpatentable over the above rejection as applied to claim 1 and further in view of Cavey (of record);
- 3) claims 21, 22, 27 under 35 USC 103(a) as being unpatentable over the above rejection as applied to claim 1, above and further in view of Wenzel et al. (of record); and
- 4) claims 10, 11 are rejected under 35 USC 103(a) as being unpatentable over the above rejection as applied to claim 9 above, and further in view of Wenzel et al. (of record);

are summarily traversed.

In this rejection, the Nishikawa is cited to disclose in connection with Fig. 36, that a tuning mechanism for an exemplary dielectric resonant element (4), includes two eccentric (i.e. offset from the center of the resonant element) cutouts or partial through holes located in the dielectric resonant element (4). The rejection further goes on to assert that a dielectric tuning body (e.g. dielectric rod 165) is insertable into and out of the cutouts to provide adjustment of the resonant frequency.

It is submitted at this point that the amount of disclosure of this embodiment *per se* is very scarce and that insertion in an out of the recesses which are found in the Fig. 36 embodiment neither discloses nor suggests the claimed rotation relative to the dielectric resonator element in order to tune the frequency of the filter.

The rotation of the dielectric rods 165 noted in this rejection totally incidental and would be understood by the hypothetical person of ordinary skill as being such. The axial displacement is

what is used to achieve the desired tuning and this would be recognized by the hypothetical person of ordinary skill. The rotation relied on for rejection is far too tainted with § 102 logic to be tenable.

Under § 103 it is necessary to show that the hypothetical person of ordinary skill would, without any knowledge of the claimed subject matter and without any inventive activity, be provided with disclosure of all of the claimed elements and then motivated to arrive at the claimed subject matter given the guidance of the cited references when each is fully considered as statutorily required.

Here, without a full working knowledge of the claimed subject matter the rotation of the rods 165 would not be given a second glance in that the rotation has no affect on the tuning of the disclosed arrangement. It is axial displacement not rotation that is the concept that would be extracted from this disclosure.

Yamakawa et al. is cited (e.g. Fig. 1(b) to discloses a dielectric resonator filter comprising dielectric resonators having a ring-like configuration (i.e. 4, 5) and a dielectric resonator having a solid disk configuration. Note is had to the configuration respect to Fig. 3(a) & Fig. 3(b), wherein there are disclosed ring-like dielectric resonator having diameter (d) and solid disk dielectric resonators having a diameter ($d^{\circ}0$), respectively. It is further asserted with respect to Figs. 6 & 7(a)-7(d), that the formation of an inner hole (i.e. in a disk shape dielectric resonator) causes the spurious frequencies to be dispersed depending on the increase in the diameter of the inner hole (e.g. see column 7, lines 1-21).

This may be so, however fails to take into account that these structures are used in combination with discs 15-20 (see Fig. 1B) which are lowered and raised in a non-contact manner with respect to the tops of the dielectric resonators 4-9.

The question is therefore, why would the hypothetical person of ordinary skill be moved to seek out the specific embodiment shown in Fig. 36 of Nishikawa et al., consider the disclosure of Yamakawa, then form holes in the cylindrical dielectric material 4 of this particular arrangement with the hope of attenuating spurious frequencies that are not disclosed as existing in this embodiment of Nishikawa, and at the same time ignore the disclosure of the disc arrangements 15-20 of Yamakawa which are lowered and raised with respect to the top of the dielectric elements in favor of the shaft 165 of Nishikawa. If the openings were of such interest would it not be more

likely that the hypothetical person of ordinary skill would simply drop Nishikawa and focus on the disclosure of Yamakawa.

The claims filed in the previous amendment stressed one main feature of the invention (each individual filter comprises a ring-like dielectric resonator element (44) with an eccentric round cutout (i.e. a cavity the axis of which does not match with the ring axis) in which a dielectric element (45) is movably disposed. This element recited as being movable about the cutout axis (60) (see more especially Fig. 12 and 13). This cutout is in the form of a circular-walled cylindrical through-hole that is concentric with respect to said axis 60).

It is submitted that neither Nishikawa nor Yamakawa discloses or suggests the use of a ring-like resonator comprising a round cutout. Although Yamakawa discloses a ring-like resonator, this resonator does not comprise any cutout (see e.g. drawing sheet 3 of 8). In the same way, Nishikawa discloses a ring-like resonator which does not comprise such a round cutout. One might say that, in the embodiment of figures 38 and 39 of Nishikawa there seems to be a ring-shaped plate (162) with cutouts, but this plate is merely an upper plate of a cylindrical metallic case (161) and the cutouts 167 made in this plate (referred to as “slits”) are not circular. Further, the elements 175 movable in these slits are not dielectric ones, but metallic nuts coupled to metallic rods 171 (column 19, lines 39 to column 20, line 2).

Since the Examiner still cites the Yamakawa and Nishikawa references as a basis for all of the rejections, there seems to be a misunderstanding with respect to the words “eccentric cutout.”

Therefore, Applicants deem it advisable to more clearly define the cutout used in the claimed subject matter. See e.g. the description in the last paragraph of page 4 (English text): it might be said that “the cutout in the dielectric resonator element is a circular cylindrical through-hole which is concentric with respect to the rotation axis, in which the external dimensions of the dielectric body are matched to the cutout in the dielectric resonator element in such a way that the two are separated from one another by only narrow air gaps”. In Nishikawa, fig. 24 to 26, as well as figure 36, obviously have nothing to do with such a definition of the resonator and of the cutouts. The same is true for fig. 1b, 3a, 3b, 6 & 7a-7d of Yamakawa.

The disclosures of Cavey, Wenzel et al. do not provide any teachings which would assist the hypothetical person of ordinary skill in coming to the conclusion purported in this Office Action to

be obvious and overcoming the above mentioned tendency to rely solely on Yamakawa rather than attempting to transfer teachings in the manner advanced in this Office Action.

Conclusion

All objections and rejections having been addressed, it is respectfully submitted that the application is in condition for allowance and a Notice to that effect is earnestly solicited.

The Examiner is invited to telephone the undersigned, Applicant's attorney of record, to facilitate advancement of the present application.

To the extent necessary, a petition for an extension of time under 37 C.F.R. 1.136 is hereby made. Please charge any shortage in fees due in connection with the filing of this paper, including extension of time fees, to Deposit Account 07-1337 and please credit any excess fees to such deposit account.

Respectfully submitted,
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Title of the Invention

TUNABLE HIGH-FREQUENCY FILTER ARRANGEMENT AND METHOD FOR
THE PRODUCTION THEREOF

5

BACKGROUND OF THE INVENTION

Field of the Invention

10 The invention relates to the field of radio-frequency engineering. It relates in particular to a tunable radio-frequency filter arrangement and to a method for its production.

15 A radio-frequency filter arrangement of this type is known, for example, from US PATENT NO. 6,147,577.

A single tunable dielectric resonator, in which the moving dielectric body can move linearly in the vertical or
20 horizontal direction in a cutout in the dielectric resonator element is known, by way of example, from EP-A1-0 601 369.

Description of the Related Art

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Transportable radio link connections (LOS=Line of Sight) have been proven for rapid and flexible construction of wire-free communication networks, in particular in rugged terrain without a suitable infrastructure, and these
30 operate in the frequency range of two or more GHz (for example 4.4 to 5 GHz; or 14.62 to 15.23 GHz). Appropriate filters, in particular bandpass filters, are required for signal processing within the transmission and reception arrangements for such directional radio links, which
35 filters are designed not only for individual frequencies

but are automatically tunable and are distinguished by constant high Q-factors over the tuning range.

In addition to the essential electrical and radio-frequency characteristics, filters of these type must, however, also be producible at low cost, must have a robust design, and must be designed to be reliable in use and to be compact and light-weight. Space (volume) and weight, in particular, are major factors for the mobility of the overall communication system.

In the past, in order to reduce the size of the cavities for filters of these type, solutions have increasingly been proposed which have a dielectric resonator element arranged in a cavity as the tunable basic element, whose resonant configuration can be varied in order to tune the filter. One such solution is described, by way of example, in US PATENT NO. 6,147,577, which was initially cited. In this known solution, a first round dielectric disk (ceramic puck) is arranged in a fixed position as a resonator in each of the cavities of the filter. An identical second round dielectric disk is located parallel above the first, and can be raised vertically, and lowered again, relative to the first disk by means of an electronically controlled motor drive. The linear movement that is required for this purpose is produced by a digital stepping motor, whose rotary movement is converted to a linear movement by a complex threaded rod mechanism.

This known filter arrangement has various disadvantages: firstly, it is comparatively difficult to achieve the comparatively high accuracy and reproducibility of the disk position during a linear movement of the moveable disk, as is required for good tunability of the filter. Secondly, the adjustment mechanism that is required for the linear

movement requires a very large amount of space. As can easily be seen from figure 4 in US PATENT NO. 6,147,577, the motorized adjustment mechanism that is arranged above the cavities occupies about 2/3 of the entire physical
5 volume of the filter. Furthermore, due to the capability of the upper disk to move in the vertical direction, the cavity must be initially designed to be comparatively large.

10 EP-A1-0 601 369, which was likewise cited initially, proposes a single tunable dielectric resonator in which an eccentric cutout is provided in the dielectric disk that is arranged in a fixed position in a cavity, which cutout can be entered to a greater or lesser extent by a dielectric
15 body that is shaped to match the cutout. The resonator is tuned by adjustment of the insertion depth. For this purpose, the dielectric body can be moved linearly via a holder in the form of a rod in the vertical direction (Figure 1 in EP-A1-0 601 369) or in the horizontal
20 direction (Figure 2 in EP-A1-0 601 369). No further details are stated about the tuning response that can be achieved by this solution. Furthermore, no mechanically adjustment mechanism is specified either, so that this proposal should in fact be regarded just as paper prior art, and its
25 feasibility is more than questionable. In particular, this solution proposal is also subject to the same disadvantages resulting from the linear movement as those which have already been discussed further above.

30 SUMMARY OF THE INVENTION

One object of the invention is thus to provide a tunable radio-frequency filter arrangement which can be produced cost-effectively, is distinguished by a particularly
35 compact and robust design with good radio-frequency

characteristics, and has an advantageous tuning response, and to specify a cost-effective and simple method for its production.

5 The essence of the invention is to provide, as a tunable filter module, a cavity with a dielectric resonator element which is arranged in a fixed position and has an eccentric cutout in which a dielectric body is arranged such that it can rotate. The arrangement of the body such that it can
10 rotate in the cutout allows the dielectric resonator element to be designed to be extremely compact. The rotary movement can be designed with high precision, thus allowing high tuning accuracy and reproducibility to be achieved.

15 One preferred refinement of the filter arrangement according to the invention is distinguished in that the dielectric resonator element is in the form of a planar, round circular disk, and in that the dielectric body can rotate about a rotation axis which is at right angles to
20 the disk plane of the dielectric resonator element, in that the dielectric resonator element has a predetermined thickness, and in that the dielectric body has a height in the direction of the rotation axis which is essentially equal to the thickness of the dielectric resonator element.

25 A development of this refinement has been found to have a particularly advantageous tuning characteristic, in which the cutout in the dielectric resonator element is a circular cylindrical through-hole which is concentric with
30 respect to the rotation axis, in which the external dimensions of the dielectric body are matched to the cutout in the dielectric resonator element in such a way that the two are separated from one another by only narrow air gaps, and the dielectric body is bounded by two parallel planar
35 surfaces in a first direction at right angles to the

rotation axis (60), and is bounded by two cylindrical envelope surfaces, which are concentric with respect to the rotation axis, in a second direction, which is at right angles to the rotation axis and to the first direction.

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Undesirable interference fields in the dielectric resonator element and in the metallic cavity are preferably suppressed by the dielectric resonator element having a central through-hole.

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It is also expedient for the dielectric resonator element and the dielectric body to be each composed of the same material.

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The filter arrangement has a particularly simple and compact design, overall, if, according to another development, the at least one filter is accommodated in a preferably rectangular filter housing, in that the filter housing is formed from a base plate and wall plates, which

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are at right angles to the base plate for the side walls, and is covered on the top face by a motor mounting plate, which is parallel to the base plate, and in that the cavities in the filter are formed by separating plates which are incorporated in the filter housing and are at

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right angles to the base plate, and mounting slots are provided in the base plate, in the wall plates and in the separating plates, by means of which the plates are plugged into one another and are connected to one another, in particular by being soldered. The electromagnetic

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interaction of the cavities is in this case achieved in a particularly simple manner in that coupling openings, in particular coupling slots, are provided at predetermined points in individual separating plates.

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Another development of the invention is distinguished in

that a preferably circular opening is provided in the motor mounting plate above each of the corresponding cavities, through which the respective dielectric resonator element and the respective dielectric body are held in the cavity, in that the dielectric resonator element and the dielectric body are part of a tuning element which is associated with the cavity and is mounted on the motor mounting plate, and in that the tuning element in each case has a fixed holder, which passes through the opening in the motor mounting plate, for the dielectric resonator element, a holder which passes through the opening in the motor mounting plate and is mounted such that it—the holder can rotate, for the dielectric body, a motor, in particular a stepping motor, and a gearbox unit, which transmits the rotational movement of the motor to the holder, ~~which is mounted such that it can rotate.~~

The arrangement is particularly compact if, according to one preferred development, the gearbox unit is accommodated in a housing, in that the housing is mounted on a motor mounting plate, in that the motor is flange-connected to the housing, and in that the holder for the dielectric resonator element is attached to the housing.

Particularly precise tuning is achieved in that the gearbox unit has a rotating element which is known in the form of a shaft, is mounted in a prestressed precision bearing and is firmly connected to the holder for the dielectric body, and in that the rotating element is driven by a drive shaft within the gearbox unit via a gearwheel which is firmly seated on the rotating element, with the drive shaft being connected to the motor and engaging with the gearwheel via a worm gear, and in that the rotating element is prestressed in the rotation direction in order to overcome play, preferably by means of a spiral spring.

Furthermore, space can be saved by the gearwheel being in the form of a circle segment, rather than a complete wheel. A configuration such as this in the form of a segment with
5 a segment angle of about 100° is completely sufficient to cover the entire worthwhile adjustment range of about 90° of the dielectric body in the cutout in the dielectric resonator element.

10 Particularly reliable tuning with high reproducibility is achieved in that, a controller, which has a control block, a memory and an input unit, is provided in the eccentric cutouts in the dielectric resonator bodies in order to control the rotation of the dielectric bodies, in that
15 position sensors, in particular in the form of light barriers which are connected to the control block, are provided in order to determine the initial position of the dielectric bodies in the radio-frequency filter arrangement, and in that value tables are stored in the
20 memory and associate an appropriate angle position of the dielectric bodies with a small number of selected frequencies of the radio-frequency filter arrangement.

One preferred refinement of the method according to the
25 invention is distinguished in that the sheet-metal parts are silver-plated, and are soldered to one another by means of a silver solder, the sheet-metal parts have mounting aids, in particular in the form of crossing slots, mounting slots and mounting lugs which are matched to one another,
30 in that the sheet-metal parts are initially loosely plugged together by means of the mounting aids and the crossing slots, mounting slots and mounting lugs in order to form the filter housing, and the plugged-together filter housing is made mechanically robust by pushing the mounting lugs
35 into the mounting slots, in that silver solder, preferably

in paste form, is applied to the junction points between the plugged-together sheet-metal parts, and in that the plugged-together sheet-metal parts are heated, preferably in an oven, until the silver solder melts and flows into
5 the junction points.

The production process is particularly simple and cost-effective if all of the sheet-metal parts of a filter housing are cut from a common metal sheet, which has not
10 been silver-plated, by means of a cutting method, preferably by means of laser cutting, in such a way that the cut-out sheet-metal parts are connected to the remaining area of the metal sheet only by a small number of narrow webs, in that the metal sheet together with the cut-
15 out sheet-metal parts is then silver-plated, in that the sheet-metal parts are detached from the metal sheet after being silver-plated, and are then used to construct the filter housing, in particular with the majority of the webs remaining at those points on the sheet-metal parts which
20 are located outside the cavities when the filter housing is complete.

BRIEF EXPLANATION OF THE FIGURES

25 The invention will be explained in more detail in the following text using exemplary embodiments and in conjunction with the drawing, in which:

Figure 1 shows a perspective overall view of the filter housing (the filter box) of a radio-frequency filter arrangement according to one preferred exemplary embodiment of the invention ~~for a total of three filters;~~
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35 Figure 2 shows the filter housing from Figure 1, in the

form of a side view of the longitudinal face with the inputs and outputs of the three filters;

Figure 3 shows the filter housing from Figure 1, in the form of a side view of the transverse face;

Figure 4 shows a perspective view of a metal sheet, which is used as a wall plate for the transverse faces of the filter housing as shown in Figure 1, ~~and has a transverse separating plate between the three filters;~~

Figure 5 shows the perspective view of a metal sheet which is used in the filter housing as shown in Figure 1 as a transverse separating plate ~~with a coupling opening between the four cavities within each of the three filters;~~

Figure 6 shows the perspective view of a metal sheet which is used in the filter housing as shown in Figure 1 as a separating plate ~~running in the longitudinal direction with coupling openings between the front and rear cavities of all three filters;~~

Figure 7 shows the perspective view of the base plate of the filter housing as shown in Figure 1 with a large number of mounting slots, ~~into which the lugs of the separating plates and wall plates as shown in Figures 2 to 5 can be inserted, and can be soldered.~~

Figure 8 shows the perspective view of a tuning unit with a motor, a gearbox unit, a dielectric resonator element and a dielectric body which can rotate;

Figure 9 shows the tuning element from Figure 8, in a view from underneath;

5 Figure 10 shows a longitudinal section through the gearbox unit of the tuning unit from Figure 8;

Figure 11 shows the perspective view of the gearwheel, which is in the form of a circle segment, from
10 the gearbox unit shown in Figure 10;

Figure 12 shows the perspective view of the dielectric resonator element of the tuning element shown in
Figure 8;

15 Figure 13 shows the perspective view of the dielectric body, which can rotate, of the tuning unit shown in Figure 8;

20 Figure 14 shows the fundamental arrangement of the cavities of a filter in a square according to the exemplary embodiment shown in Figure 1, ~~and the orientation of the associated dielectric resonator elements and bodies within the~~
25 ~~cavities, with respect to the coupling slots;~~

Figure 15 shows an alternative arrangement to that in Figure 14 of the cavities of a filter, in a row;

30 Figure 16 shows the outline circuit diagram of a control system for the radio-frequency filter arrangement according to the invention;

Figure 17 shows the arrangement and configuration of the
35 sheet-metal parts for a filter housing as shown

in Figure 1 on a common metal sheet;

Figure 18 shows the relationship between the filter frequency of the filter according to the exemplary embodiment and the rotation angle of the dielectric body 45;

Figure 19 shows the measured frequency profile of the S parameters S11 (reflection coefficient at the input; curve B) and S21 (transmission coefficient in the forward direction; ~~curve A) of the filter according to the exemplary embodiment for the tuned frequency of 4.7 GHz over a frequency range of ± 15 MHz about the respective mid frequency,~~ and

Figure 20 shows the measured frequency profile of the S parameter S21 of the filter according to the exemplary embodiment, ~~for the tuned frequency of 4.7 GHz over a wider frequency range of ± 60 MHz about the respective mid frequency.~~

DETAILED DESCRIPTION OF THE EMBODIMENTS OF THE INVENTION

The tunable radio-frequency filter arrangement which is described in the following text has a filter housing (10 in Figure 1) in which a number of tuning units (40 in Figure 8) are inserted and are screwed to the motor mounting plate (13 in Figure 1). The filter housing and the tuning units will be explained separately. The completely assembled filter arrangement is not illustrated, for reasons of clarity.

The rectangular filter housing (filter box) 10 illustrated in Figure 1 is composed of a thicker (at the top) motor mounting plate 13 and of a number of sheet-metal parts, which form the base, side walls and (inner) separating walls of the filter housing 10. The sheet-metal parts include the baseplate 11, which is illustrated individually in Figure 7, the wall plates 12 and 20 (see also Figure 4) which run in the transverse direction, the wall plates 14 and 32 (Figures 1, 2 respectively) which run in the longitudinal direction, the transverse (inner) separating plates 15, ~~17, 19~~, 19 which are illustrated ~~individually in Figures 4 and in Fig. 5~~, and the (inner) separating plate 33, which is located in the longitudinal direction and is illustrated individually in Figure 6. The sheet-metal parts are composed, for example, of 1 mm thick silver-plate sheet steel (material No. 1.4301). The motor mounting plate 13 is composed of the same material and is likewise silver-plated, but has a thickness of, for example, 4 mm.

As can be seen from Figure 17, the sheet-metal parts can be produced particularly easily and cost-effectively by cutting all of the sheet-metal parts of the filter housing 10 out of a common metal sheet 69 of suitable size, in the manner illustrated in Figure 17. First of all, the metal sheet 69 is not silver-plated. Initially, the contours of the required sheet-metal parts 11, 12, 14, ..., 20, 32 and 33 are cut out in the metal sheet 69 by laser cutting and by a comparable cutting technique, with the sheet-metal parts that have been cut out still being connected to the rest of the metal sheet 69 at various points by narrow webs. The majority of the webs are arranged at points on the sheet-metal parts which are located outside the cavities 21, ..., 24 in the subsequent filter housing 10. The lack of any silver layer at these points means that there will be no affects on the radio-frequency characteristics of the

cavities. Once the cut metal sheet 69 is in the form shown in Figure 17, a silver layer is provided over its entire surface. This results in the sheet-metal parts being virtually completely silver-plated. Such silver plating is missing only in the areas of the webs which will later be cut through. However, since these are largely located outside the cavities, this is not disadvantageous.

The filter housing 10 is formed from the individual sheet-metal parts 11, 12, 14,...,20; 32, 33 and the motor mounting plate 13 by soldering and pinning. The soldering is carried out by means of a suitable silver solder in an oven. The sheet-metal parts 11, 12, 14,...,20; 32, 33 are for this purpose first of all provisionally connected by plugging mounting lugs and mounting slots that are provided for this purpose into one another, and the sheet-metal housing that is formed is made mechanically robust by pushing the mounting lugs into the mounting slots. Only the wall plates 14, 32 on the longitudinal face of the filter housing 10 are pinned at the upper edge to the end faces of the motor mounting plate ~~11~~13. A suitable amount of solder in the form of solder paste is applied to the junction points between the sheet-metal parts and is distributed such that the gaps at the junction points are reliably closed during the soldering process. The housing that has been prepared in this way is then heated in an oven to the temperature required for soldering, and is cooled down again once the solder has melted and has run in the junction points.

In order to plug the sheet-metal parts 11, 12, 14,...,20; 32, 33 into one another, the baseplate 11 and the wall plates 14, 32 which are arranged on the longitudinal faces of the housing are , as shown in Figure 7, provided with a number of mounting slots 39 (some of which cross). The wall

plates 12, 14, 20 and 32 and the separating plates 15,...,19 and 33 are equipped on their lower edges with mounting lugs L1 (Figures 4, 5 and 6) appropriate for this purpose, by means of which they can be plugged through the mounting
5 slots 39 in the baseplate 11, and can be soldered. The transverse wall plates 12 and 20 and separating plates 15,...,19 additionally have mounting lugs L2 (Figures 4 and 5) on their side edges, which can be plugged through corresponding mounting slots in the longitudinal wall
10 plates 14, 32, and can be soldered. In order to allow unimpeded crossing of the transverse wall and separating plates 12, 14,...,20; ~~32~~—with the longitudinally running separating plate 33, special crossing slots 34, 36, 37 and 38 (Figures 4-6) are provided in these sheet-metal parts.
15 In this case, the crossings are alternate on the upper face and lower face (alternating crossing slots 37, 38 in Figure 6).

The longitudinally running separating plate 33 and the
20 transverse separating plates 15,...,19 result in a total of $3 \times 4 = 12$ identical cavities, each with a square base area (A1, A2, A3, A4 in Figure 7) being formed in the filter housing 10, four associated cavities of which are annotated, by way of example, with the reference symbols
25 21,22, 23, 24 in Figure 1. The four associated cavities 21,22, 23, 24 which are arranged in a square form a filter F3. In addition to the filter F3, the filter housing 10 shown in Figure 1 has two further identical filters F2 and F1 which likewise each comprise four cavities arranged in a
30 square. Each of the filters F1, F2 and F3 as shown in Figure 2 has an associated input 26, 28, 30, and an output 27, 29, 31, respectively.

The four cavities of each of the filters F1, F2 and F3 are
35 coupled to one another for radio-frequency purposes. This

is achieved by means of suitably arranged, elongated coupling slots 35 in the transverse separating plates 15, 17, and 19 (Figure 5) and in the longitudinally running separating plate 33 (Figure 6). The coupling slots 35 are
5 positioned in the present example such that they are located in the center of the wall of the adjacent cavity and on the vertical center plane of the cavities to be coupled. The importance of this position for the coupling characteristics will be described in more detail later. The
10 transverse separating plates 16 and 18 which separate the filters F1, F2 and F3 from one another are, of course, not equipped with coupling openings.

A circular dielectric resonator element 44 (Figure 12) in
15 the form of a disk is arranged in the center of each of the cavities 21,...,24 formed in the filter housing 10 and governs the overall radio-frequency and transmission characteristic of the individual cavity and of the respective filter. The dielectric resonator element 44 is
20 part of a compact tuning unit 40 that is associated with each cavity (Figures 8-10). The tuning unit 40 is screwed onto the robust motor mounting plate 13 from above and has a fixed holder 46 (Figure 10), to end of which the dielectric resonator element 44 is attached, which projects
25 through a (circular) opening 25 (Figure 1), which is associated with the cavity, into the cavity located underneath.

The dielectric resonator element 44 has a central circular
30 through-hole 58 and an eccentrically arranged circular cutout 59 (Figure 12). A dielectric body 45 (Figure 13) of the same thickness is mounted in the eccentric cutout 59 such that it can rotate about a rotation axis 60 that is at right angles to the disk plane of the dielectric resonator
35 element 44. The cutout 59 is in the form of a circular-

cylindrical through-hole that is concentric about the rotation axis 60. The external dimensions of the dielectric body 45 are matched to the cutout 59 in such a way that the two are separated from one another only by narrow air gaps.

5 For this purpose, the dielectric body 45 is bounded in a first direction (which is at right angles to the rotation axis 60) by two parallel, planar surfaces 61, 62, and is bounded in a second direction (which is at right angles to the rotation axis 60 and to the first direction) by two
10 cylindrical envelope surfaces 63, 64, which are concentric about the rotation axis 60 (see Figure 13; the body 45 inserted into the cutout can be seen in Figure 9).

The dielectric body 45 is preferably formed from the same
15 dielectric material as the dielectric resonator element 44. It is attached to the end of a holder 47 (Figure 10) which is mounted such that it can rotate, and can be rotated by means of the mechanism that is accommodated in the tuning unit 40 relative to the dielectric resonator element 44,
20 about the rotation axis 60. The rotation allows the resonant frequency of the resonator element, and thus the mid-frequency of the filter, to be varied.

The tuning unit 40 (Figures 8-10) essentially comprises a
25 gearbox unit 42 and a motor 41, which is flange-connected to the gearbox unit 42 (see Figure 10) at the side and drives the holder 47 (which can rotate) via the gearbox unit 42. The motor 41 is preferably a stepping motor. As can be seen from Figure 10, the gearbox unit 42 has a
30 housing 43 on whose lower face the holder 46 for the stationary dielectric resonator element 44 is mounted. A rotating element 49 in the form of a shaft is mounted by means of a precision bearing 48 such that it can rotate in a through-hole which passes through the base of the housing
35 43 at right angles, and this rotating element 49 is firmly

connected to the holder 47 that can rotate. By way of example, a special bearing which can be prestressed, is provided with two ball bearings and is used in hard disk memories of PCs is used as the precision bearing 48.

5 Bearings of this type can be obtained, for example, using the name "RO bearing" (after the inventor Rikuro Obara from the Japanese Company Minebea Co, Ltd. Their principle is described inter alia, in US PATENT NO. 5,556,209. The precision bearing 48 contributes to the achievement of a
10 positioning accuracy of the dielectric body 45 in the region of a few micrometers, as is required for accurate tuning of the filters F1, F2 and F3.

A gearwheel 51 in the form of a circle sector is mounted on
15 the rotating element 49, as shown in Figure 11. Since the full tuning range of the configuration shown in Figure 9 and comprises the dielectric resonator element 44 and the dielectric body 45 can be covered by rotation of the body through 90° from the position shown in Figure 9, a sector
20 angle of 100° is more than adequate for the gearwheel 51. Designing the gearwheel 51 to be in the form of a circle sector means that the gearbox unit 42 and thus the tuning unit 40 can be designed to be extremely compact

The worm gear on a driveshaft 55 (Figure 10), which is at
25 right angles to the rotation axis 60 and is connected directly to the motor 41, engages with the gearwheel 51. In order to ensure that there is no play in the engagement between the worm gear and the gearwheel 51, the rotating element is prestressed in the rotation direction by means
30 of a spiral spring 50, which is mounted on the housing 43. Two light barriers 52 and 53 are provided in the gearbox unit 42, in order to control the drive unit 40. The first light barrier 52 scans a marking element (not shown in Figure 10) which is in the form of a rod, is seated in an
35 appropriate mounting hole 56, 57 in the gearwheel 51

(Figure 11) and marks the end points of the pivoting range. The second light barrier 53 scans a position sensor disk 54, which is seated on the driveshaft 55 and is provided with a radial slot. The interaction of the two light
5 barriers allows the initial or zero position of the gearwheel 51, and thus the initial position of the dielectric body 45, to be determined precisely.

As already mentioned further above, the four cavities 21,
10 22, 23, and ~~24~~ with the dielectric resonator elements 44 and bodies 45 placed centrally in them are arranged in a square in each of the filters F1, F2 and ~~F3~~ (see Figure 2). This is illustrated once again in Figure 14 on the basis of the example of the filter F3. The RF energy is
15 injected into the first cavity 21, propagates by means of the coupling slots 35 via the adjacent cavities 22, 23 and 24, and is emitted again from the last cavity 24. The coupling slots 35 are located on the vertical center planes or in the center of separating walls of the cavities
20 21,...,24. The dielectric resonator elements 44 are rotated together with their eccentric cutouts 59 from the vertical center plane of the coupling slot 35 that is located closest to the cutout through a predetermined angle which, in the example, is about 57°. This particular configuration
25 of the cutout and coupling slot results in the filter having a radio-frequency response in which the coupling factor decreases as the frequency increases, when the dielectric body 45 is rotated toward the next coupling slot. An additional degree of freedom is provided by the
30 capability for additional coupling between the first cavity 21 and the last cavity 24, as is indicated by the S-shaped coupling element in Figure 14.

Another configuration of a filter F' by means of which -
35 apart from the transverse coupling - the same effect can be

achieved is for the cavities 21,...,24 to be arranged as shown in Figure 15. In this case as well, the coupling slots 35 are arranged centrally, and the dielectric resonator elements 44 are rotated, together with their
5 cutouts, through about 60° from the center plane.

A control system is provided for tuning of the filter arrangement by means of the tuning elements 40, and a highly simplified block diagram of this control system is
10 illustrated in Figure 16. The controller 65 has a control block 66 which, for example, has a suitable microprocessor and a number of power outputs corresponding to the number of motors 41. The control block 66 controls the stepping motors 45 via the power outputs, and is activated from the
15 outside via an input unit 68. The control block 66 interacts with a memory (EPROM) 67, in which value tables are stored, which associate a specific step number of the stepping motors 41 with a number of selected frequency values of the filter. Intermediate values are produced by
20 interpolation. Furthermore, the control block 66 receives signals from the two light barriers 52, 53 for each tuning unit 40. If a specific frequency for the filter or filters is intended to be set (during start-up), the dielectric bodies 45 are first of all moved back to their initial
25 position. The reaching of the initial position is signaled by appropriate signals from the two light barriers 52, 53. The stepping motors 41 are then switched forward from the initial position by the number of steps corresponding to the table value taken from the memory 67, or to a value
30 determined by interpolation for the desired frequency. The motors 41 for a filter may in this case all be switched largely at the same time, or may be switched following a specific algorithm.

35 If the radio-frequency filter arrangement with the filter

housing 10 according to the exemplary embodiment (Figure 1) is intended to be designed for ~~band 4, that is to say for a~~ tunable frequency range from about 4.4 GHz to 5 GHz, the housing (without the tuning units) has a base area of approximately 66 mm × 186 mm, and a height of approximately 30 mm. Each of the cavities has a base area (A1,...,A4 in Figure 7) of 28 mm × 28 mm, and a height of 20 mm. The dielectric resonator element 44 has a thickness of approximately 6 mm, an external diameter of approximately 15 mm, and an internal diameter of approximately 6.5 mm. The diameter of the eccentric cutout 59 is approximately 6 mm, the width of the dielectric body 45 between the parallel vertical boundary surfaces is approximately 3 mm. The tuning unit 40 projects only approximately 24 mm beyond the surface of the motor mounting plate 13.

Characteristic curves as are shown in Figures 18 to 20 are obtained for a filter arrangement designed in this way:

Figure 18 shows the relationship between the tunable filter frequency and the rotation angle of the dielectric body 45 in the eccentric cutout 59 in the dielectric resonator element 44. The rotation angle range is from 0° to 90°. At 0° the straight sides of the dielectric body 45 are tangential with respect to the dielectric resonator elements 44.

Figure 19 shows the measured curves for a number of S parameters of the filters according to the exemplary embodiment, specifically the reflection coefficient at the input S11 (curve B), the transmission coefficient in the forward direction, S21 (curve A), as a function of the frequency for a selected mid-frequency of 4.7 GHz. The frequency range is in this case ± 15 MHz about the respective mid-frequency. The graph is logarithmic. The

scale in the vertical direction is 0.5 dB per division for S21, and 5 dB per division for S11.

Figure 20 shows the measured curve for S21 for 4.7 GHz over an extended frequency range of ± 60 MHz about the respective mid-frequency. The graph is logarithmic. In this case, the scale in the vertical direction is 10 dB per division.

Overall, the invention provides a tunable radio-frequency filter arrangement which can be designed such that it is simple and costs little, can be tuned very accurately and reproducibly over a wide frequency range, is extremely compact, and is distinguished by very good radio-frequency characteristics. In particular, a number of identical filters can be accommodated in a common filter housing, with little additional complexity.

List of reference symbols

20	10	Filter housing (Filter box)
	11	Base plate
	12, 20	Wall plate (transverse)
	13	Motor mounting plate
	14, 32	Wall plate (longitudinal)
25	15, 17 and 17 , 19	Separating plate (transverse)
	21, 22, 23, and 24	Cavity
	25	Opening (Circuit)
	26, 28, 30	Input (Filters F1, F2, F3)
	27, 29, 31	Output (Filters F1, F2, F3)
30	33	Separating plate (longitudinal)
	34, 36, 37, 38	Crossing slot
	39	Mounting slot
	35	Coupling slot
	40	Tuning unit
35	41	Motor (stepping motor)

	42	Gearbox unit
	43	Housing (Gearbox unit)
	44	Dielectric resonator element (stationary)
5	45	Dielectric body (moving)
	46	Holder (in the form of a half shell)
	47	Holder (which can rotate)
	48	Precision bearing
	49	Rotating element
10	50	Spiral spring
	51	Gearwheel (in the form of a circle segment)
	52, 53	Light barrier
	54	Position sensor disk
15	55	Drive shaft (with worm gear)
	56, 57	Attachment hole (position sensor pin)
	58	Central through-hole
	59	Eccentric cutout
	60	Rotation axis
20	<u>61, 62, 63 and 64</u>	Boundary surface
	65	Controller
	66	Control block
	67	Memory (EPROM)
	68	Input unit
25	69	Metal sheet
	<u>A1, A2, A3 and A4</u>	Surface
	F, F1, F2, F3	Filter (Bandpass filter)
	K1, K2	Curve
	L1, L2	Mounting lug